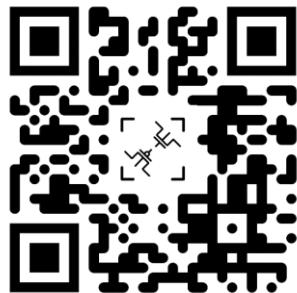


Advanced Compact MOSFET Model: Design-oriented ACM2 model

20/06/2024



Deni Germano Alves Neto

denialves77@gmail.com

[https://github.com/ACMmodel/MOSFET model](https://github.com/ACMmodel/MOSFET_model)

“Scan me”

About me

- Universidade Federal de Santa Catarina – UFSC - Brazil $V_{DD} < 100 \text{ mV}$
- Undergrad and Masters in IC design - 2022
 - Subject : Ultra-Low-Voltage IC circuits
 - Dissertation: Ultra-Low-Voltage Standard Cell Library
 - ACM for low voltage circuits
- First contact with open-source IC design :
 - Chipathon - SSCS 2021 :
 - Analog-front-end for Biosignals – AFEbio
- Start PhD in 2023 : MOSFET Modeling
- Joint PhD between UFSC and Université Grenoble Alpes (Currently based)
 - Chipathon-SSCS & UNIC-CASS 2023 – Analog IC design
 - Live demonstration of the ACM2 at ISCAS 2024 with the open-source tools (XSCHEM)



Outline

- **Introduction: Compact models**
- ACM2 model vs V_{GS} model
- ACM2 model vs PSP
- Parameter extraction and circuit example

What is a compact model ?

- Compact Model is the medium of information exchange between foundry and designer.
- Provides **detailed information** about device operation & characteristics
- However, needs to be:
 - **Simple** enough to be incorporated in circuit simulators
 - **Accurate** enough to predict behavior of circuits

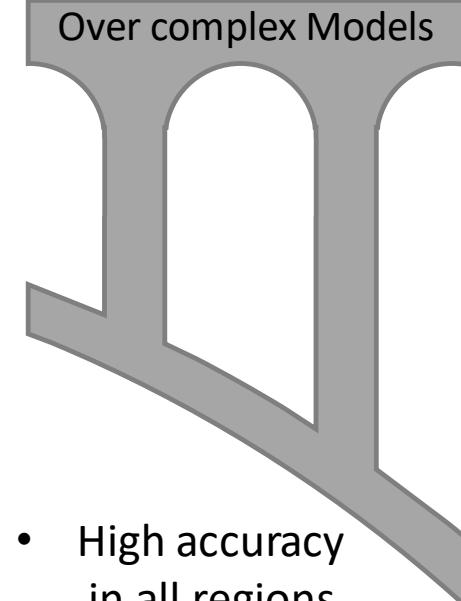
Why the need for a design-oriented MOSFET model ?

- Provides a proper bridge between the electrical behavior of the MOSFET and circuit performance through simple analytical equations
- Allows analytical sizing of the transistors
- Avoids excessive dependency of the IC designer in using parametric simulations with complex models to define the operation point!



Oversimplified models

- Poor accuracy, only in one region
- 2/3 DC parameters



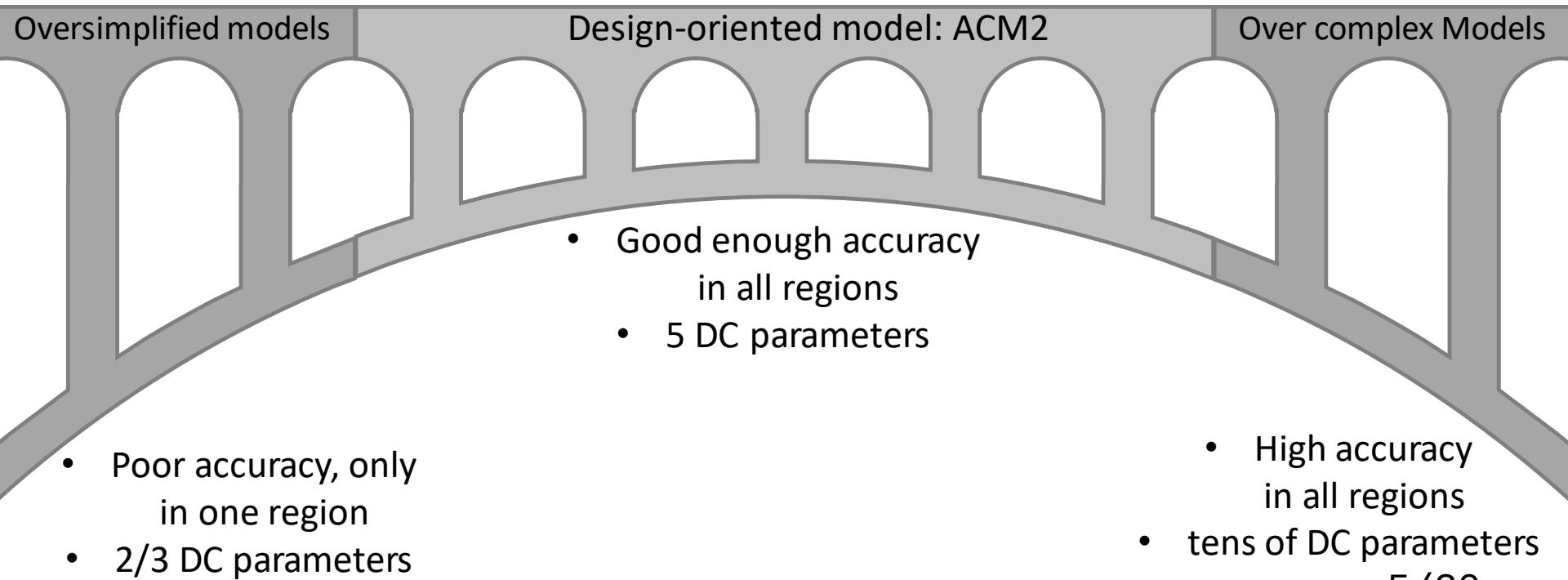
Over complex Models

- High accuracy in all regions
- tens of DC parameters

Why the need for a design-oriented MOSFET model ?

- Provides a proper bridge between the electrical behavior of the MOSFET and circuit performance through simple analytical equations
- Allows analytical sizing of the transistors
- Avoids excessive dependency of the IC designer in using parametric simulations
- **Increase the designer intuition!**

IC designers bridge



Open-Source IC design

Open-source PDK



Open-source EDA tools



Few open-source IP & libraries



Available compact MOSFET models



We propose:

ACM2 : A Simple 5-DC-parameter MOSFET model



ACM2: A simple 5-DC-parameter MOSFET model

Complete Continuous All-region charge-based MOSFET model

$$V_P = \frac{V_{GB} - V_{T0} + \sigma(V_{DB} + V_{SB})}{n}$$

$$\frac{V_P - V_{SB}}{\phi_t} = q_s - 1 + \ln(q_s)$$

$$q_{dsat} = q_s + 1 + \frac{1}{\zeta} - \sqrt{\left(1 + \frac{1}{\zeta}\right)^2 + \frac{2q_s}{\zeta}}$$

$$\frac{V_{DS}}{\phi_t} = q_s - q_d + \ln\left(\frac{q_s - q_{dsat}}{q_d - q_{dsat}}\right)$$

$$I_D = I_S \frac{(q_s + q_d + 2)}{1 + \zeta(q_s - q_d)} (q_s - q_d)$$

- Used to calculate q_s
- Bridge between **WI** and **SI** regions

- Used to calculate q_d
- Bridge between **Triode** and **Saturation** regions

Specific current
 I_S

Threshold voltage
 V_{T0}

Slope factor
 n

DIBL factor
 σ

V_{sat} effect
 ζ

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Inversion charges in terms of the inversion levels

Unified Charge Control Model

$$\frac{V_P - V_{S(D)B}}{\phi_t} = q_{s(d)} - 1 + \ln q_{s(d)}$$

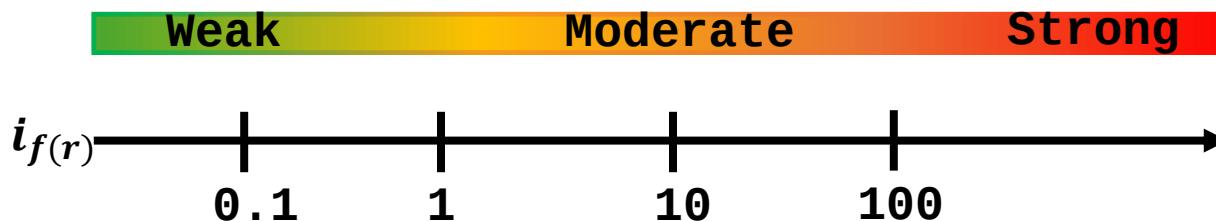
Relationship between normalized inversion charge and inversion level: $q_{s(d)} = \sqrt{1 + i_{f(r)}} - 1$

Unified (I)current Control Model

$$\frac{V_P - V_{S(D)B}}{\phi_t} = \sqrt{1 + i_{f(r)}} - 2 + \ln\left(\sqrt{1 + i_{f(r)}} - 1\right)$$

$$\frac{I_D}{I_S} = \frac{I_F - I_R}{I_S} = i_f - i_r$$

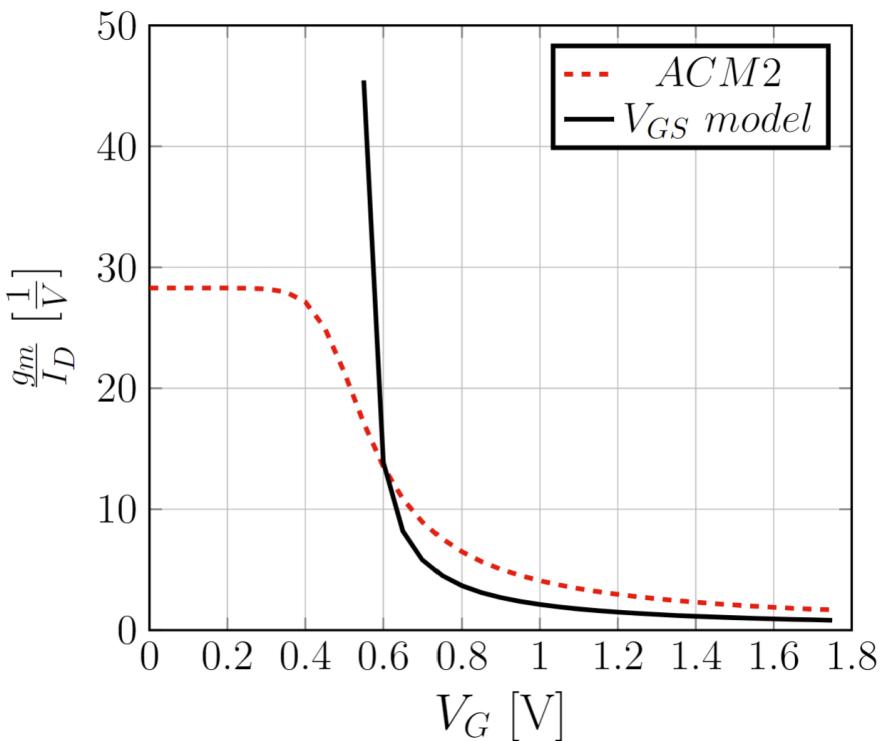
→ $i_{f(r)}$ is the forward (reverse) inversion level



Oversimplified model vs ACM-3PM model @ Saturation

$$I_D = \frac{\beta}{2} (V_{GS} - V_T)^2$$

$$\frac{g_m}{I_D} = \frac{1}{V_{GS} - V_T}$$



$$i_f = \frac{I_D}{I_S} \quad V_P = \frac{V_{GB} - \textcolor{blue}{V}_{T0}}{\textcolor{blue}{n}}$$

$$\frac{V_P - V_{S(D)B}}{\phi_t} = \sqrt{1 + i_f} - 2 + \ln\left(\sqrt{1 + i_f} - 1\right)$$

$$\frac{g_m}{I_D} = \frac{2}{n\phi_t(\sqrt{1 + i_f})}$$

Misconception about overdrive voltage:
NMOS example:

$$V_{OV} = V_{GS} - V_T$$



$$V_{OV} = V_P - V_{SB} = \frac{V_{GB} - V_T}{\textcolor{red}{n}} - V_{SB}$$



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Physics-based saturation: design model

Normalized saturation current
due to velocity saturation of
carriers

$$i_{dsat} = \frac{2}{\zeta} q_{dsat}$$

Normalized current vs.
normalized charge densities

$$\frac{I_D}{I_S} = i_{dsat} = \frac{(q_s + q_{dsat} + 2)}{1 + \zeta(q_s - q_{dsat})} (q_s - q_{dsat})$$

$$q_{dsat} = q_s + 1 + \frac{1}{\zeta} - \sqrt{\left(1 + \frac{1}{\zeta}\right)^2 + \frac{2q_s}{\zeta}}$$

$$\zeta = \frac{(\mu_s \phi_t / L)}{v_{sat}}$$

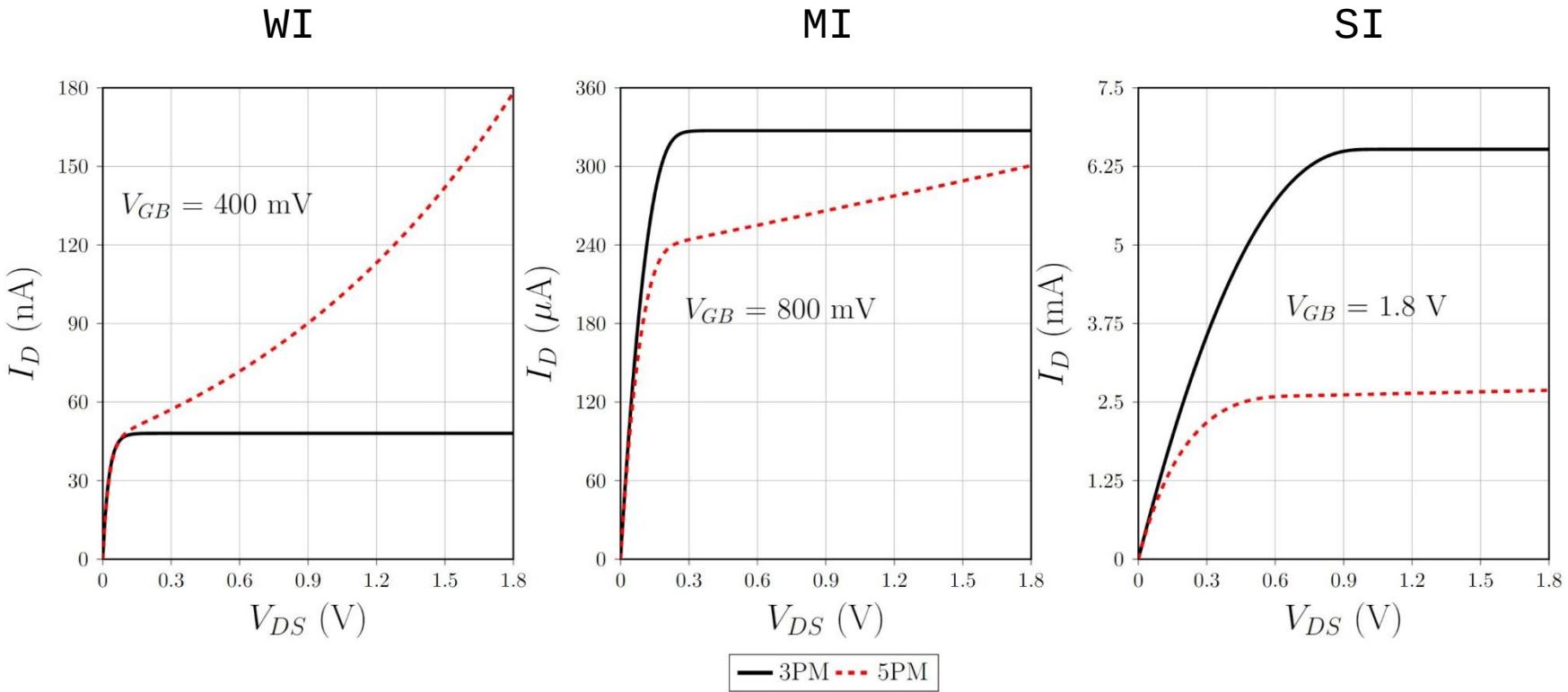
or, equivalently

$$q_s = \sqrt{1 + \frac{2}{\zeta} q_{dsat}} - 1 + q_{dsat}$$

Unified Charge Control Model including the effect of *velocity saturation*

$$\frac{V_{DS}}{\phi_t} = q_s - q_d + \ln \left(\frac{q_s - q_{dsat}}{q_d - q_{dsat}} \right)$$

Output characteristics including DIBL and v_{sat}

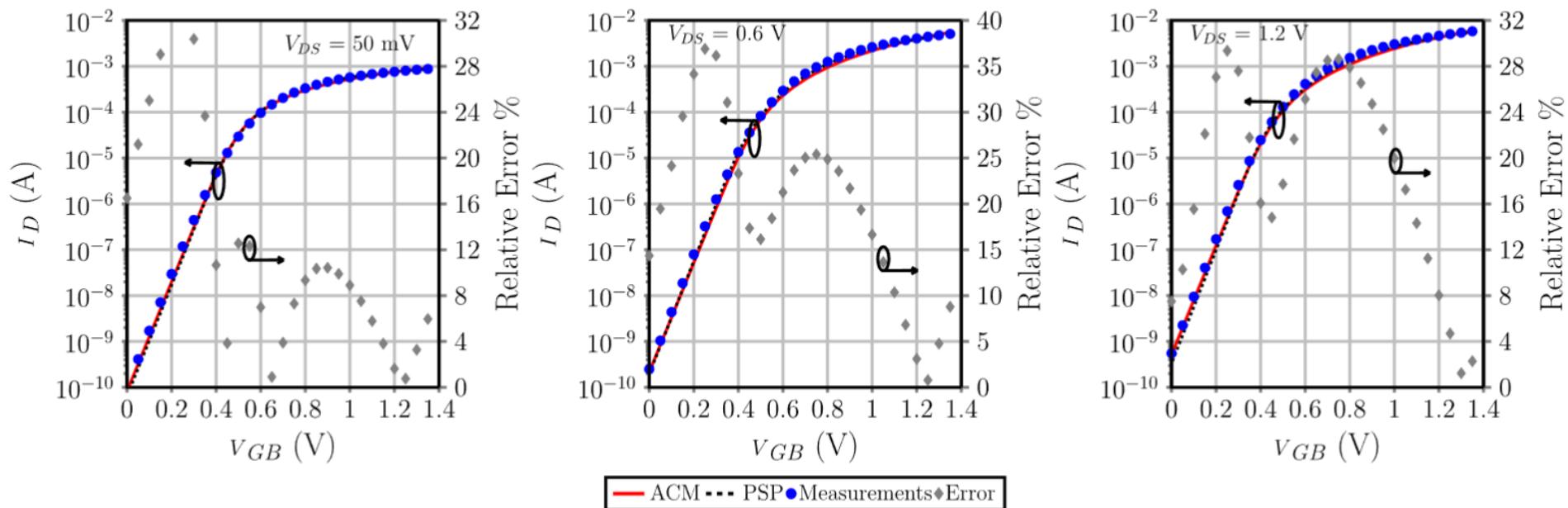


$$DIBL \text{ model: } V_T = V_{T0} - \sigma(V_{SB} + V_{DB})$$

Transistor	W/L [μ m]	V_{T0} [mV]	I_S [μ A]	n	σ	ζ
NMOS	5/0.18	528	5.52	1.37	0.025	0.056

ACM2¹ vs PSP – 130 nm SiGe IHP²

I_D vs V_{GB}



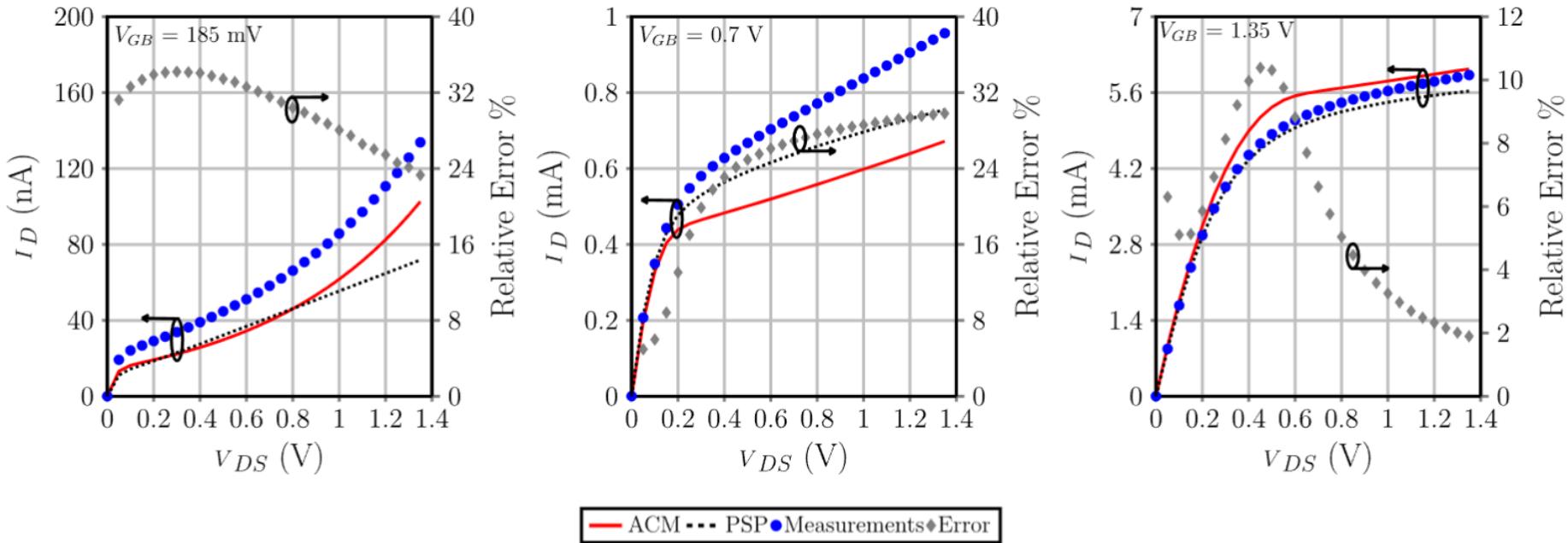
Characteristics of a LVT NMOS bulk transistor with $W/L = 10\mu\text{m}/120 \text{ nm}$.

¹ ACM2 : implemented in verilog-A, compiled by OPENVAF, simulated in Ngspice

² Institut for High-Performance Microelectronics (IHP) open-source PDK

ACM2¹ vs PSP – 130 nm SiGe IHP²

I_D vs V_{DS}



Characteristics of a LVT NMOS bulk transistor with $W / L = 10 \mu\text{m} / 120 \text{ nm}$.

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3PM-ACM model in a nutshell

$$I_D = I_S [i_f - i_r] \quad \text{where} \quad I_S = \mu C_{ox} n \frac{\phi_t^2 W}{2 L} = I_{SH} \frac{W}{L}$$

$$\frac{V_P - V_{S(D)B}}{\phi_t} = \sqrt{1 + i_{f(r)}} - 2 + \ln\left(\sqrt{1 + i_{f(r)}} - 1\right) \quad V_P \cong \frac{V_{GB} - V_{T0}}{n}$$

DC eqs

If we choose $i_f = 3 \rightarrow V_{GB} = V_{T0}$

$$\frac{V_{DS}}{\phi_t} = \sqrt{1 + i_f} - \sqrt{1 + i_r} + \ln\left(\frac{\sqrt{1 + i_f} - 1}{\sqrt{1 + i_r} - 1}\right)$$

$$g_{ms(d)} = \frac{2I_S}{\phi_t} \left(\sqrt{1 + i_{f(r)}} - 1 \right) \rightarrow \frac{W}{L} = \frac{g_{ms(d)} \phi_t}{2I_{SH} (\sqrt{1 + i_{f(r)}} - 1)}$$

$$g_m = \frac{g_{ms} - g_{md}}{n}$$

$$\frac{g_m}{I_D} = \frac{d(\ln I_D)}{dV_G} = \frac{2}{n \phi_t (\sqrt{1 + i_f} + \sqrt{1 + i_r})}$$

Small - signal eqs

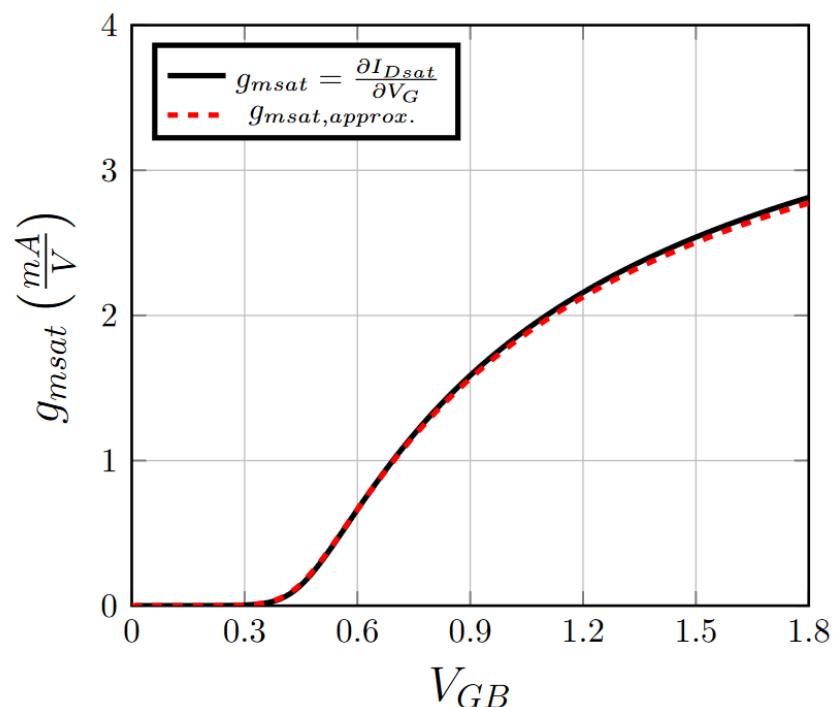
5PM-ACM2 : Transconductances in saturation

$$I_D = \frac{2I_S}{\zeta} q_{dsat} \quad \text{where}$$

$$g_m \triangleq \frac{\partial I_D}{\partial V_G} \quad g_{md} \triangleq \frac{\partial I_D}{\partial V_D}$$

$$\left\{ \begin{array}{l} I_S = \mu C_{ox} n \frac{\phi_t^2}{2} \frac{W}{L} = I_{SH} \frac{W}{L} \\ q_{dsat} = q_s + 1 + \frac{1}{\zeta} - \sqrt{\left(1 + \frac{1}{\zeta}\right)^2 + \frac{2q_s}{\zeta}} \end{array} \right.$$

$$\left\{ \begin{array}{l} g_m(q_s) \\ \quad g_m = \frac{2I_S}{n\phi_t} \frac{q_s}{1 + \zeta(q_s + 1)} \\ \quad g_{m3} = \frac{16I_S}{(n\phi_t)^3} \frac{q_s}{(q_s + 1)^3} \frac{2 - 2\zeta q_s - 3\zeta q_s^2}{(q_s + 1)^4} \\ \\ g_m(i_{dsat}) \\ \quad g_m = \frac{2I_S}{n\phi_t} \frac{(\sqrt{1 + i_{dsat}} - 1)}{\zeta \sqrt{i_{dsat}}} \end{array} \right.$$



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- **ACM2 model vs PSP**
- **Parameter extraction and Circuit example**

I_S , V_{TO} and n extraction

The g_m/I_D method

Let us choose: $V_{DS} = \phi_t/2$ and $i_f = 3$

$$\rightarrow \frac{V_{DS}}{\phi_t} = \sqrt{1 + i_f} - \sqrt{1 + i_r} + \ln\left(\frac{\sqrt{1 + i_f} - 1}{\sqrt{1 + i_r} - 1}\right)$$

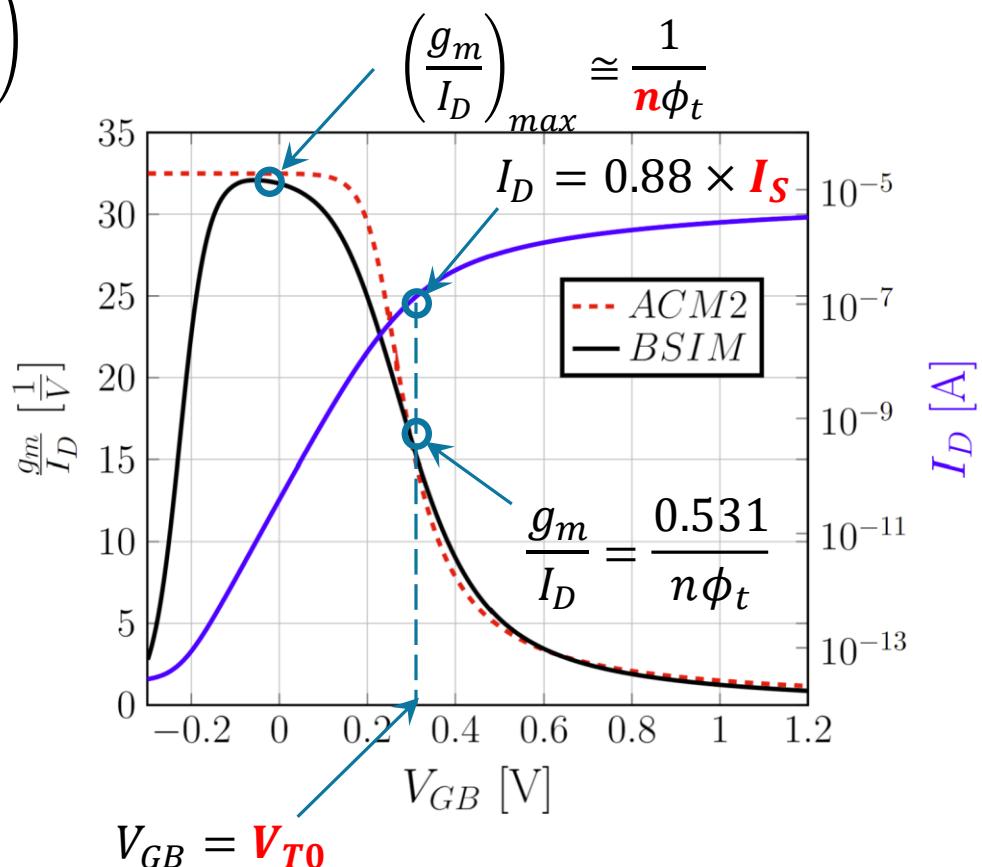
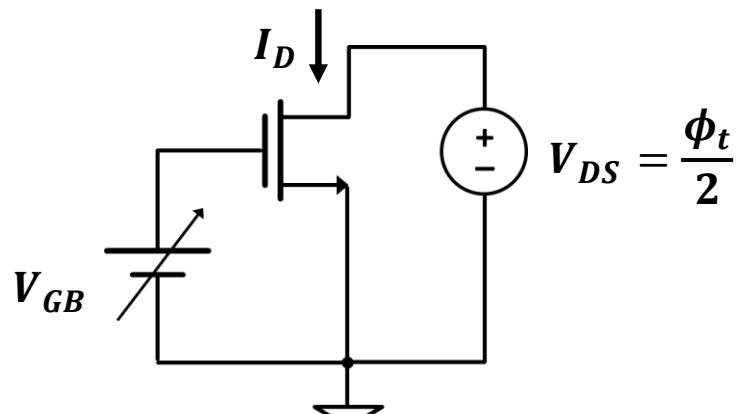
Thus : $i_r = 2.12$

$$\rightarrow \frac{g_m}{I_D} = \frac{d(\ln I_D)}{dV_G} = \frac{2}{n\phi_t(\sqrt{1 + i_f} + \sqrt{1 + i_r})}$$

$$\frac{g_m}{I_D} = \frac{0.531}{n\phi_t} = 0.531 \left(\frac{g_m}{I_D} \right)_{max}$$

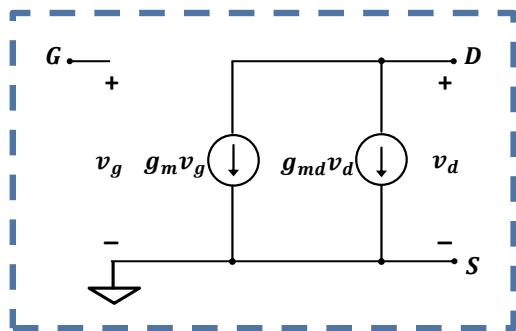
$$\rightarrow I_D = I_S(i_f - i_r)$$

$$I_D = (3 - 2.12) I_S = 0.88 I_S$$

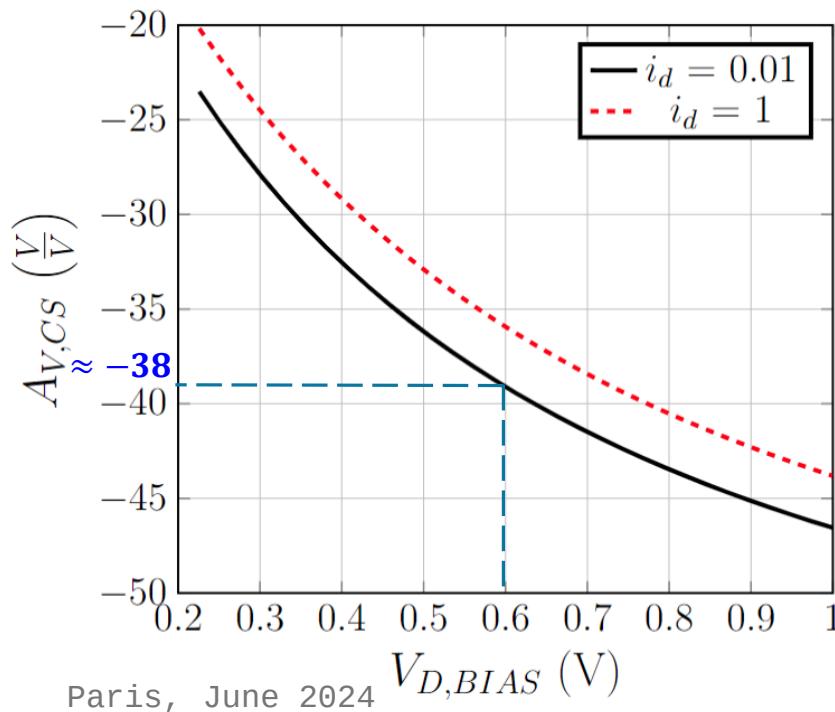
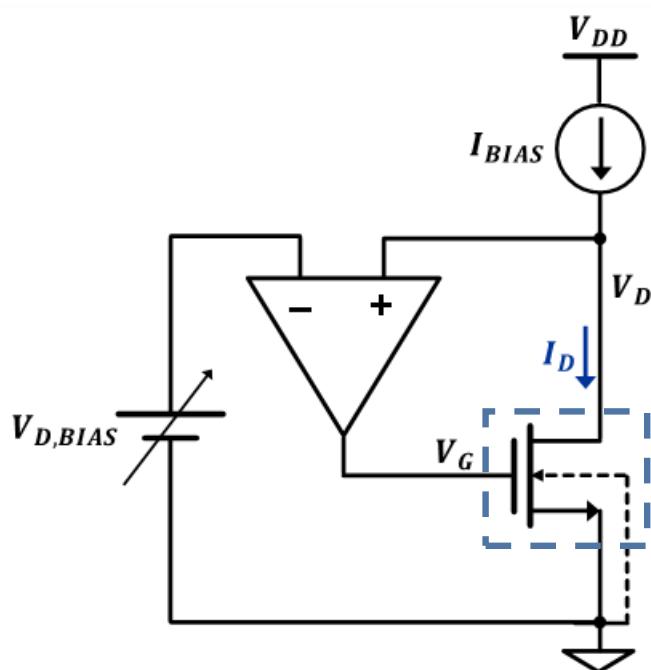


Extraction of σ

Common-Source Intrinsic-Gain method



$$A_{V,CS} = \frac{v_d}{v_g} = -\frac{g_m}{g_{md}} = -\frac{\frac{g_m}{I_{D,sat}}}{\frac{g_{md}}{I_{D,sat}}} = -\frac{\frac{1}{\phi_t} \left(\frac{1}{n}\right) \frac{2}{1 + \sqrt{1 + i_f}}}{\frac{1}{\phi_t} \left(\frac{\sigma}{n}\right) \frac{2}{1 + \sqrt{1 + i_f}}} = -\frac{1}{\sigma}$$



$$A_{V,CS} = -\frac{1}{\sigma}$$

$$\sigma = -\frac{1}{(-38)}$$

$$\sigma = 0.026$$

ζ extraction

$$i_{dsat} = \frac{2}{\zeta} q_{dsat}$$

$$q_s = \sqrt{1 + \frac{2}{\zeta} q_{dsat}} - 1 + q_{dsat}$$

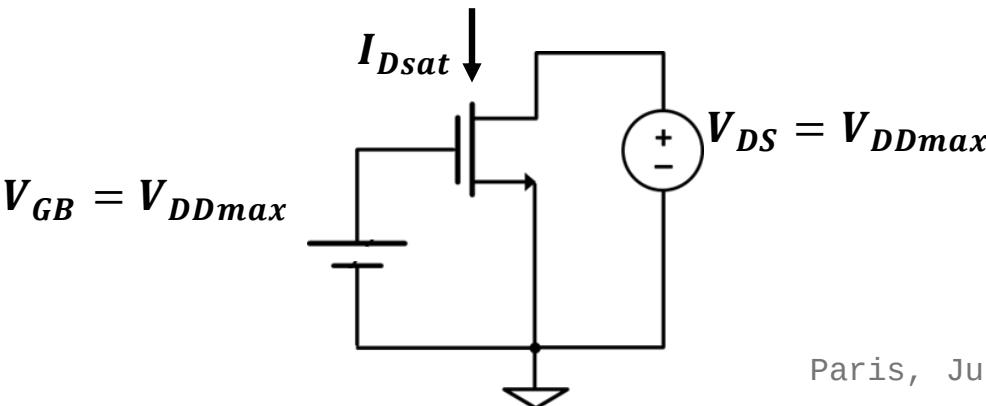
$$\zeta = \frac{2(q_s + 1 - \sqrt{1 + i_{dsat}})}{i_{dsat}}$$

- q_s calculated using parameters (V_{T0} , n , σ) and UCCM.



$$V_P = \frac{V_{GB} - V_{T0} + \sigma(V_{DB} + V_{SB})}{n}$$

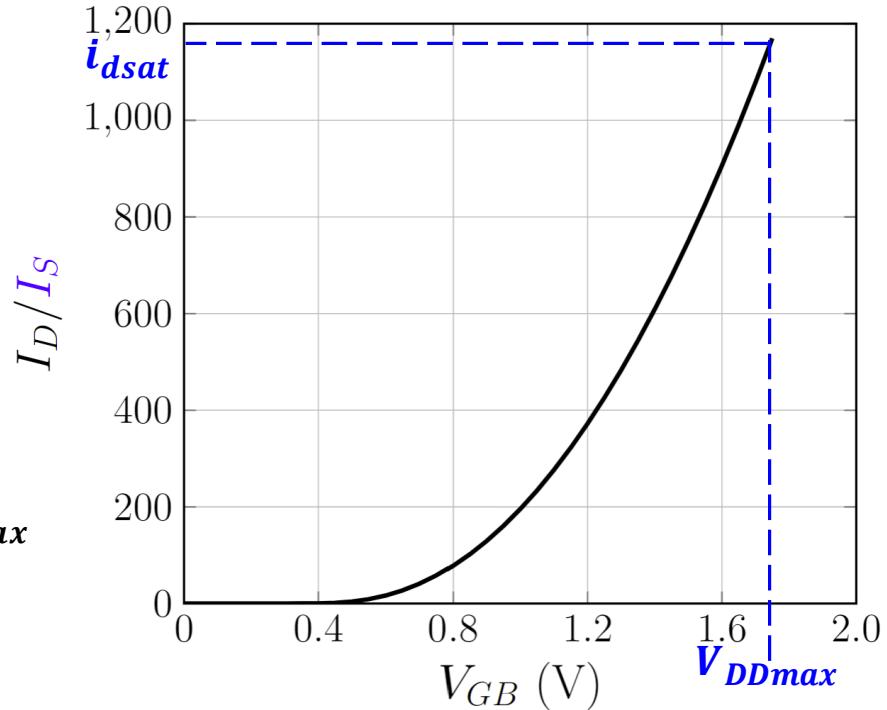
$$\frac{V_P - V_{S(D)B}}{\phi_t} = q_s - 1 + \ln(q_s)$$



- Measure

$$I_{Dsat} = I_D(V_G = V_D = V_{DDmax} \text{ and } V_S = V_B)$$

$$i_{dsat} = I_{Dsat}/I_S.$$

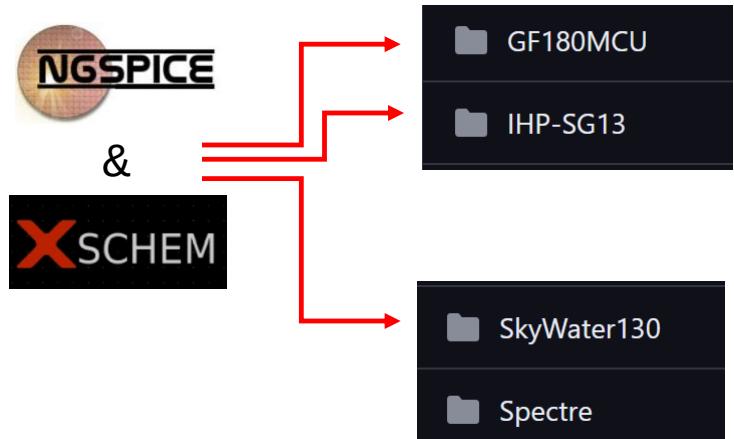


Github – ACM2

Github - Content

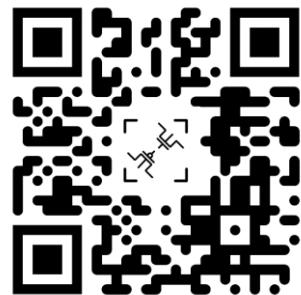


Examples of PDKs and circuit simulators using the ACM model

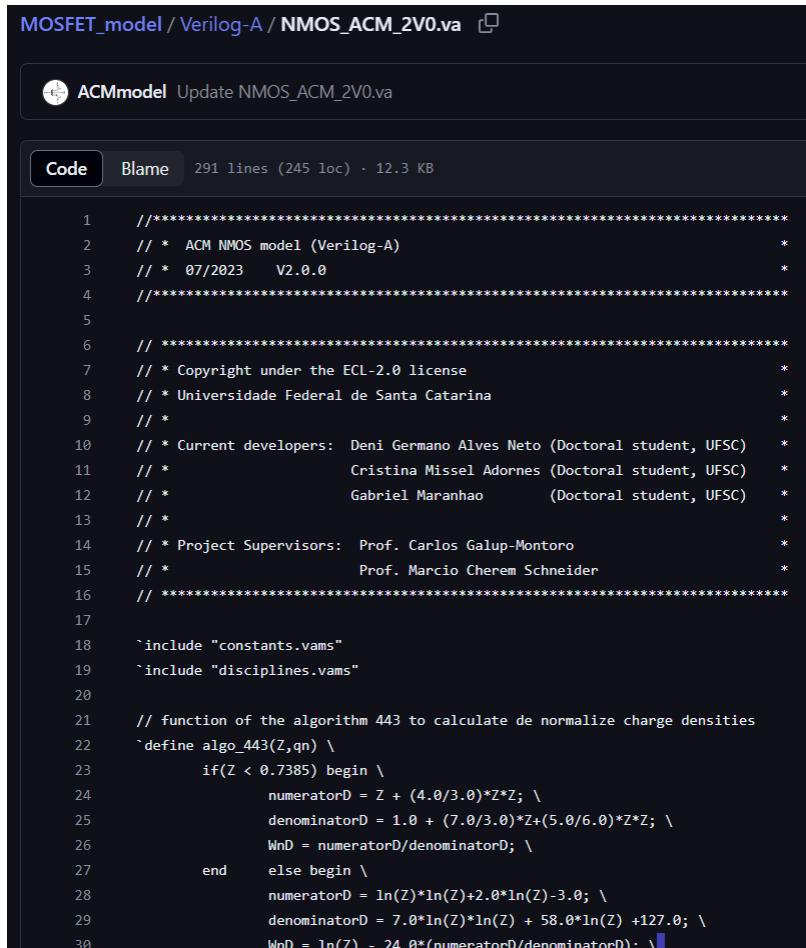


Paris, June 2024

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Verilog-A code Available!



Automatic parameter extraction – IHP @ Xschem

ACM2 MOSFET Model

→ ACM2 Model Report
→ Github

IHP SG13G2 130nm
BiCMOS Open Source PDK

NMOS Extraction

V_{t0}, I_S, n
nmos_ext
x1

sigma
nmos_sigma_ext
x2

zeta
nmos_zeta
x3

PMOS Extraction

V_{t0}, I_S, n
pmos_ext
x4

sigma
pmos_sigma_ext
x5

zeta
pmos_zeta
x6

TestBenchs

ACM2 vs. PSP - nfet IHP 130 nm
TB_nmox_acm
x7

ACM2 vs. PSP - pfet IHP 130 nm
TB_pmos_acm
x8



ACM2 MOSFET Model Authors

2024-04-17 21:28:31

/home/gmaranhao/Documents/MOSFET_model/Examples/IHP-SG13/xschem/ACM2_Extraction.sch



Also, available for GF180 and SKY130

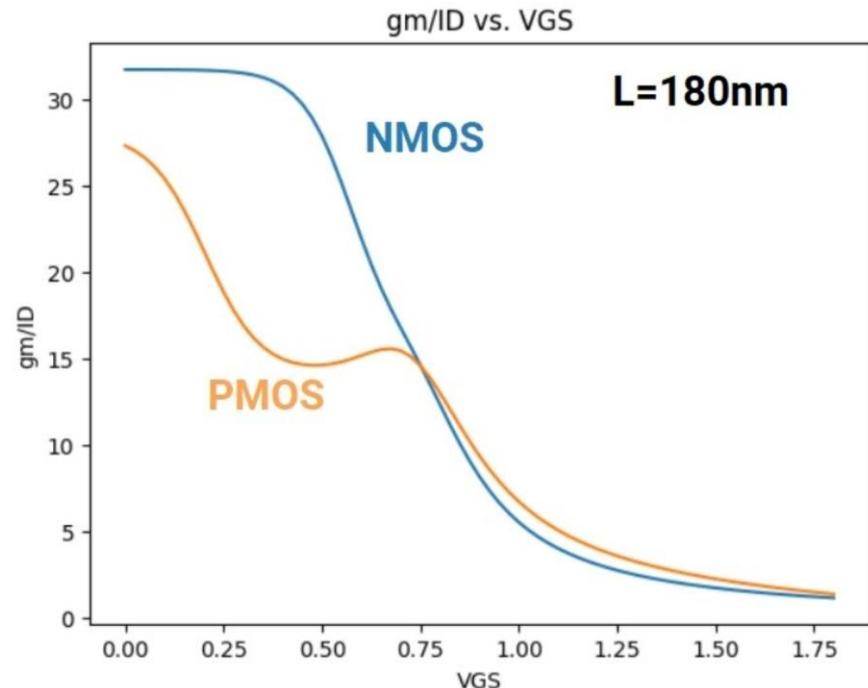
Automatic parameter extraction - "ACM2PDK"

- Dependency of the parameters

$$V_{T0}, I_S, n, \sigma, \zeta$$

- Control Voltages- V_G, V_D, V_S, V_B
- Geometry - W & L
- Temperature
- Corners

BSIM4 issues in sky130

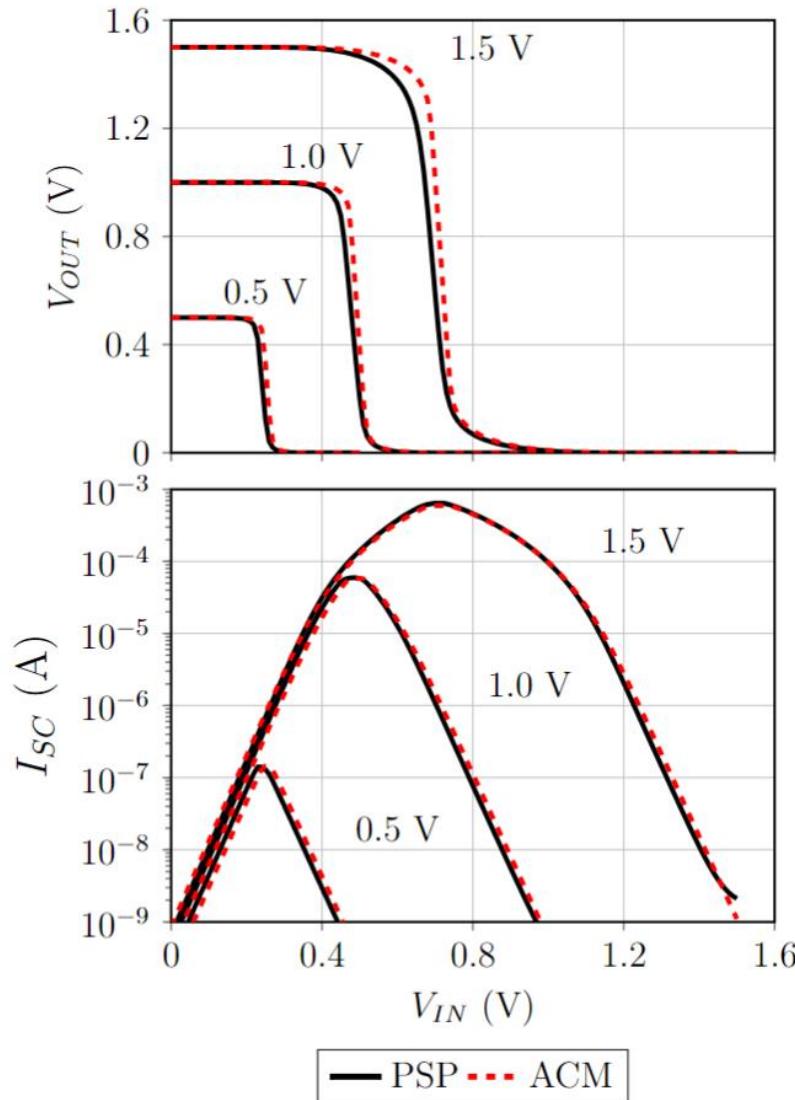
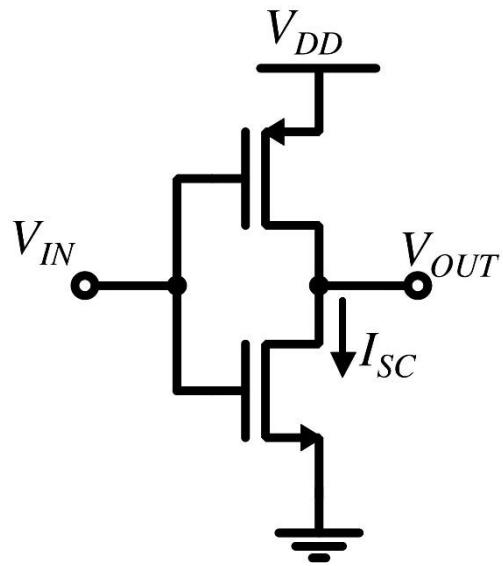


Thanks Tim Edwards for the
sky130 samples

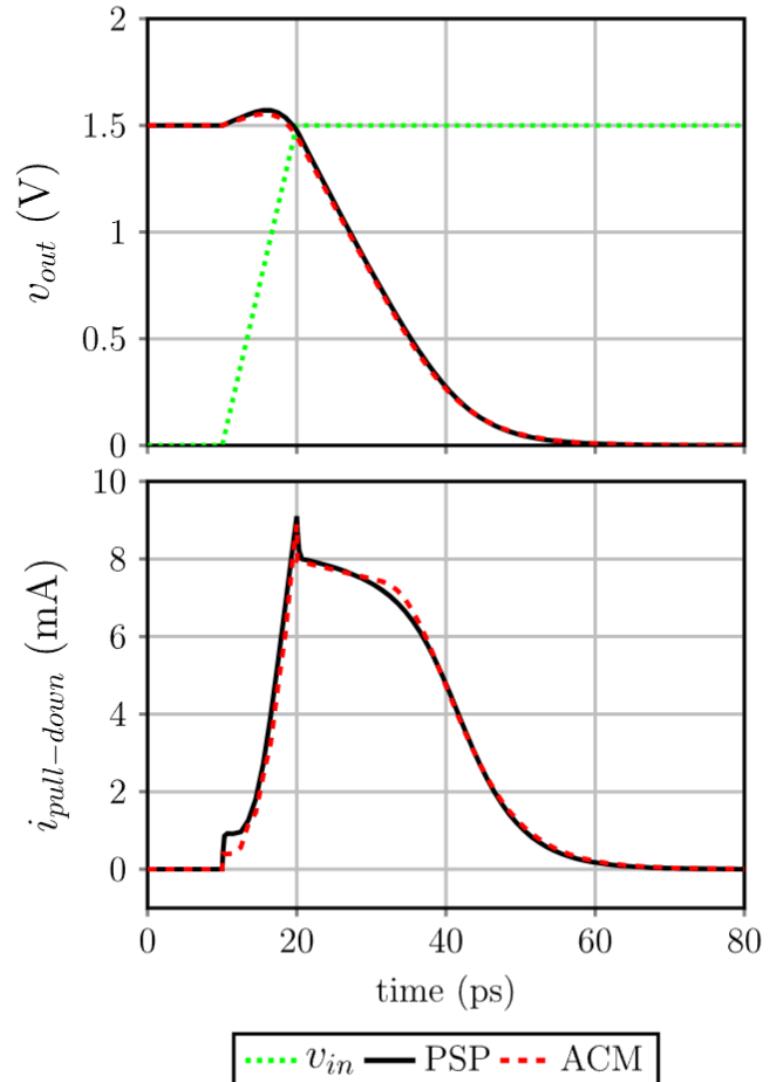
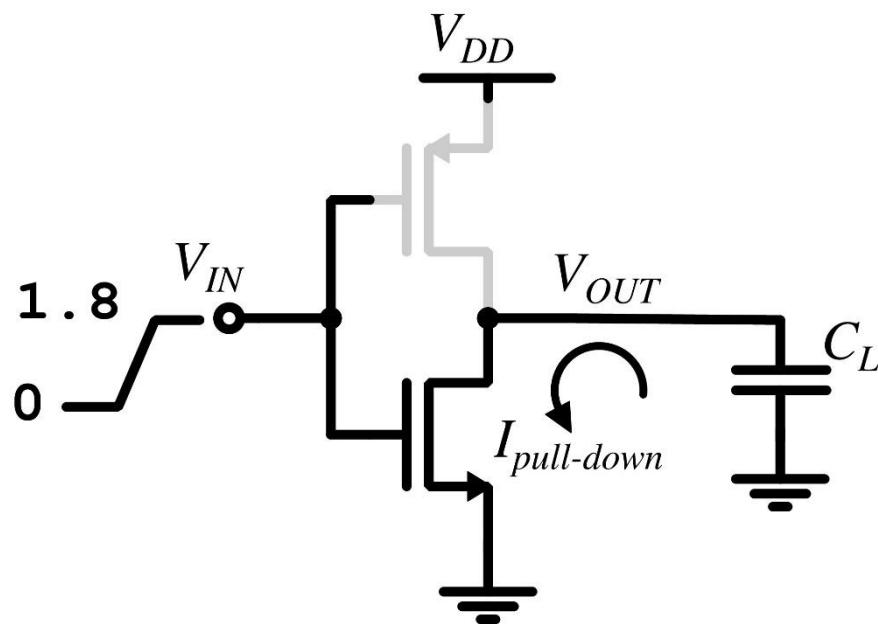
We need more samples to do measurements!
And Funding!

CMOS Inverter in 130 nm bulk

VTC and short-circuit current



CMOS Inverter in 130 nm bulk Output Voltage and pull-down current



Summary – The ACM2 model

- *A truly compact MOSFET model with single-piece functions*
- *Implemented in Verilog-A for simulation*
- *Interchangeable between simulators (SPICE or SPECTRE)*
- *Verify in all three open-source PDKs (Sky130, GF180, IHP-SG13G2)*
- *Helpful to designers (only 5-DC-parameters)*
- *Simplified parameter extraction procedure*
 - *Accepts parameters extracted from simulations or chip measurements*

Acknowledgments

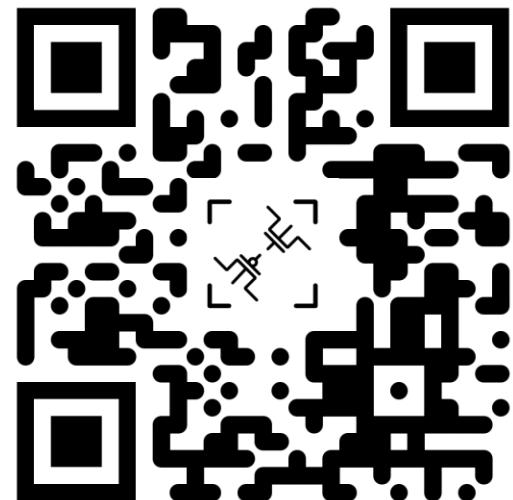
- **LCI-UFSC, Florianopolis, Brazil**
- **TIMA, Univ. Grenoble Alpes, France**
- **IHP, Frankfurt Oder, Germany**
- **Efabless**
- **STIC-AmSud multinational program**
- **CAPES and CNPq agencies, Brazil**

References

- D. G. Alves Neto, C. M. Adornes, G. Maranhão, M. K. Bouchoucha, M. J. Barragan, A. Cathelin, M. C. Schneider, S. Bourdel, C. Galup-Montoro, A 5-DC-Parameter MOSFET Model for Circuit Simulation in QucsStudio and Spectre, Newcas 2023.
- ACM2 Github: https://github.com/ACMmodel/MOSFET_model
- IHP Github : <https://github.com/IHP-GmbH/IHP-Open-PDK>

“Scan me”

- Available in Github:
 - DC model
 - Small-signal model
 - Dynamic model
 - Thermal & Flicker noise models (1/f)

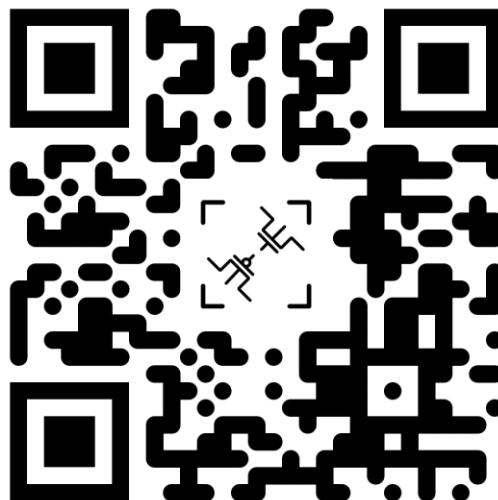


What's next?

- Introduction to open-source IC design at UFSC
- Short design course in



Questions ?



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