High-Sensitivity Split-Contact Magnetoresistors on Lightly Doped Silicon Substrates

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Abstract—In this paper we show that silicon split-contact magnetoresistors with geometric dimensions of the order of the Debye length (L_D) can have much higher sensitivities than the usual devices with much larger length and width than L_D . Numerical simulations carried out with Comsol Multiphysics show that silicon n-type magnetoresistors with dimensions of the order of L_D can have magnetic sensitivity as high as 60%/T which is ten times higher than usual sensitivities.

I. INTRODUCTION

When a Hall plate is immersed in a magnetic field perpendicular to its plane, galvanomagnetic effects occur due to the Lorentz force acting on charge carriers [1]. The output signal can be a Hall voltage or a current imbalance. In the latter case, Split-Contact Magnetoresistors (SC-MR) [2]–[4] or split-contact magnetotransistors [1] are the usual devices.

Hall plates have been numerically modeled and experimentally characterized with many technologies and geometric shapes [5], [6]. However, the Hall plates usually studied have geometrical dimensions much larger than the Debye length (L_D) . The reported experimental results show that the silicon SC-MR sensitivity is around 6 % of relative current imbalance /Tesla [2]–[4], [6], [7].

This work shows that it is possible to significantly increase the sensitivity of silicon SC-MRs using dimensions of the order of the Debye length. Numerical simulations carried out with COMSOL Multiphysics [8] enabled to confirm a simple analytical model of the sensitivity as a function of the ratio (geometric dimensions)/ L_D .

This paper is organized as follows. Section II introduces the split-contact magnetoresistor and the definition of a current deflection quality parameter. Section III presents a simple analytical model of the current imbalance due to the magnetoresistance effect, Section IV summarizes the numerical simulation model, Section V discusses the simulation results, and finally, conclusions are given in Section VI.

II. SPLIT-CONTACT MAGNETORESISTORS

A standard rectangular SC-MR is a Hall plate with split contacts as shown in Fig, 1. Its active area is L in length and W in width, and the separation between contacts is dd. The sensitivity, S, of such devices is usually defined as

$$S = \frac{|I_{C2} - I_{C1}|}{(I_{C1} + I_{C2})B} 100\% = \frac{|\Delta I|}{IB} 100\%$$
(1)

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Figure 1. Schematic view of a standard rectangular split-contact magnetoresistor.

where $I_{C1}-I_{C2} = \Delta I$ is the current imbalance, $I_{C1}+I_{C2} = I$ is the total current, and B is the intensity of the magnetic field perpendicular to the magnetoresistor active area.

The importance of the current-line deflection effect in the performance of a SC-MR can be characterized using the normalized deflection-quality factor J_{DQn} defined as [9]:

$$J_{DQn}(x) = \frac{L_{ci}}{(W - dd) \left| \overline{J}_{Bx-L} \right| B} \left| J_{By-ls} \right| 100\%$$
 (2)

where J_{By-ls} is the lateral current density on the line of symmetry, \overline{J}_{Bx-L} is the average longitudinal current density on the contacts C1 and C2 (at x = L), and L_{ci} is the SC-MR length where the current imbalance due to the current-line deflection effect is generated.

III. ANALYTICAL MODEL

In an *n*-type SC-MR, the magnetic part of the Lorentz force $F_{Lm} = -q(v_d \times B)$, where v_d is the carrier drift velocity, concentrates charge carriers on a lateral side. Therefore, this side of the plate becomes negatively and the opposite positively charged, as Figure 2 shows [1]. The width of these charged regions are of the order of the Debye length L_D since it is the characteristic distance over which large departure from neutrality occurs in a uniformly doped material in equilibrium.

To obtain a simple analytical model, let us assume that the excess of electron density Δn and the defect of electron density $-\Delta n$ on each lateral side of the plate are constant over the lateral distance mL_D (see Fig. 2), where m is a



Figure 2. Current-lines deflection effect and variation of the carriers concentration on the lateral sides of a SC-MR in regions with extensions of the order of the Debye length L_D .

positive proportional factor. Applying the Gauss theorem, the Hall electric field E_H is

$$E_H = \frac{q \,\Delta n \,m \,L_D}{\epsilon_s} \tag{3}$$

where m is a positive number, q is the elementary charge and ϵ_s is the silicon permittivity.

The Hall electric field is $E_H = G \mu_{Hn} E_x B$, where G is the geometric correction factor [1], μ_{Hn} is the Hall mobility for electrons, $E_x = V_b/L$ is the longitudinal component of the electric field and V_b is the bias voltage (see Fig. 2). Applying these expressions in Equation 3, we obtain

$$\Delta n = \mu_{Hn} B \frac{\epsilon_s}{q} \frac{V_b}{L m L_D} G(L, W, L_D) \tag{4}$$

From the definition of $L_D = \sqrt{kT \epsilon_s/q^2/n}$, where k is the Boltzmann's constant and T is the absolute temperature, the electrons concentration is

$$n = \frac{kT}{q^2} \frac{\epsilon_s}{L_D^2} \tag{5}$$

Then, from Equations 4 and 5, we obtain

$$\frac{\Delta n}{n} = \mu_{Hn} B \frac{V_b}{\frac{kT}{q}} \frac{L_D}{mL} G\left(L, W, L_D\right) \tag{6}$$

On the other hand, the normalized current imbalance generated by the excess and defect of electrons in the lateral regions of width mL_D , is

$$\frac{\Delta I}{I} = 2 \frac{\Delta n}{n} \frac{m L_D}{W} \tag{7}$$

Then, from Equations 6 and 7, $\Delta I/I$ can be expressed as

$$\frac{\Delta I}{I} = 2\,\mu_{Hn} B \frac{V_b}{\frac{kT}{q}} \frac{L_D^2}{L W} G\left(L, W, L_D\right) \tag{8}$$

Equation 8 shows that the magnetoresistance effect is proportional to the ratio $L_D^2/(LW)$. Let us consider, as an example, a doping concentration of $N_D = 10^{15} \, cm^{-3}$ for which the Debye length is $L_D = 130 \, nm$. For geometric dimensions as large as $100 \, \mu m$, $L_D^2/(LW)$ is of the order of 10^{-6} while for dimensions of the order of L_D (such as 100 nm), $L_D^2/(LW)$ is of the order of the unity. The last case can be realized in advanced technologies such as FDSOI, where the doping concentration is $N_A = 10^{15} cm^{-3}$ [10]. Thus, the magnetoresistance effect in FDSOI can be 6 orders of magnitude higher than in conventional technologies.

IV. NUMERICAL SIMULATION

In this work, *n*-type SC-MR were studied. Poisson's equation and the continuity equation for electrons were solved in COMSOL Multiphysics 4.2a [8]

$$-\nabla \cdot (\epsilon \nabla \Psi) = q \left(p - n + N_D - N_A \right) \tag{9}$$

$$-\frac{1}{q}\nabla \cdot J_{nB} = -R_{SRH} \tag{10}$$

where Ψ is the electrostatic potential, p and n are the holes and electrons concentrations, respectively, N_D and N_A are the donors and acceptors concentrations, respectively, J_{nB} is the current density for electrons and R_{SRH} is the Shockley-Read-Hall generation-recombination ratio.

Considering an isothermal and stationary process with a magnetic field B = 1T perpendicular to the magnetoresistor area, the total current density for electrons is

$$J_{nB} = (J_{n0} - \mu_{Hn} (J_{n0} \times B)) \left(1 + (\mu_{Hn}B)^2\right)^{-1} \quad (11)$$

where J_{n0} is the current density for electrons under a zero magnetic field. $J_{n0} = -q n \mu_n \nabla \Psi + q D_n \nabla n$ where μ_n is the electron mobility and D_n is the electron diffusion constant [1].

Dirichlet boundary conditions for the electrostatic potential, Ψ , and for electron density at ideal contacts (C1, C2 and C3) are considered (see Fig. 1). At the remaining boundaries, the normal components of electron current density and the field strength are assumed to be zero.

V. RESULTS

Applying a bias voltage $V_b = 5 V$, SC-MRs with aspect ratio L/W from 0.5 to 4, electrons concentrations $N_D = 5E13 \ cm^{-3}$ and $N_D = 5E17 \ cm^{-3}$ and contacts split $dd = 0 \ \mu m$ and $dd = 0.4 \ \mu m$ immersed in a magnetic field of $1 \ T$ were modeled in COMSOL Multiphysics [8]. A constant mobility $\mu_n = 1000 \ cm^2/V/s$ was considered.

For $N_D = 5E13 \, cm^{-3}$, the current and equipotential lines of SC-MRs with non-ideal split contacts $dd = 0.4 \, \mu m$ and an aspect ratio L/W = 4 are shown in Figure 3. The Debye length L_D for this value of N_D is $\approx 0.574 \, \mu m$. Figure 3(a) shows the case when $L = 3 \, \mu m$ and $W = 0.75 \, \mu m$, and Figure 3(b) shows the case when $L = 20 \, \mu m$ and $W = 5 \, \mu m$. In the first case, the current-lines deflection effect is more important than in the second one, due to the dimensions of the SC-MR are in the order of L_D . For the same reason, the variation of the electrons concentration n is more important in the first case than in the second one as Figure 4 shows.

According to [9], the sensitivity due to the current-lines deflection effect can be calculated by the average value of



Figure 3. Current and equipotential lines in split-contact magnetoresistors with non-ideal split contacts $dd = 0.4 \,\mu m @ N_D = 5E13 \, cm^{-3}$, L/W = 0.4 and $B = 1 \, T$.

the normalized deflection-quality factor J_{DQn} . Figure 5 shows the values of J_{DQn} for non-ideal split contacts $dd = 0.4 \, \mu m$ with $N_D = 5E13 \, cm^{-3}$ and L/W = 4. The average value of J_{DQn} for $L = 3 \, \mu m$ and $L = 5 \, \mu m$ is around $30 \, \%/T$, but the sensitivity for these cases are $45 \, \%/T$ and $48 \, \%/T$, respectively. As a result, the current-lines deflection effect is not sufficient to characterize the sensitivity of SC-MR with dimensions of the order of the Debye length.

As Figure 4 shows, the variation of the electrons concentration on the lateral sides of a SC-MR is also important when its dimensions are of the order of L_D which also contributes to the current imbalance (see Equation 7).

Figure 6 compares the cases of SC-MRs with ideally split and non-ideally split contacts. The sensitivity of a SC-MR decreases when its contacts are non-ideally split. In order to analyze the impact of the aspect ratio L/W on the sensitivity, SC-MRs with ideally split contacts were considered. The sensitivity of these SC-MRs decreases when the aspect ratio L/W decreases from 4 to 0.5 as Figure 7(a) shows.

Figure 7(b) compares the sensitivities of square devices with low $(N_D = 5E13cm^{-3})$ and high $(N_D = 5E17cm^{-3})$ doping. As it is clear from Figure 7(b), the sensitivity of a high doped device is the same as for a hundred times larger low doped device. Thus, the sensitivity is a function of L/L_D and W/L_D . Consequently, the function G in Equations 4, 6 and 8 has the form

$$G = G\left(\frac{L}{L_D}, \frac{W}{L_D}\right) \tag{12}$$

VI. CONCLUSIONS

Simulation results show that the the sensitivity of Split-Contact Magnetoresistors (SC-MR) is a function of their geometric dimensions normalized to the Debye length (L_D) . High-sensitivity SC-MRs are obtained when their width and length are of the order of L_D . For these devices, the carriers



(a) $L = 3 \, \mu m$



(b) $L = 20 \, \mu m$

Figure 4. Electrons concentration in split-contact magnetoresistors with nonideal split contacts $dd = 0.4 \,\mu m @ N_D = 5E13 \, cm^{-3}$, L/W = 0.4 and $B = 1 \, T$.

concentration variation can produce a current imbalance more intense than the one produced by the current-lines deflection effect. Numerical simulation results show that sensitivities up to 60 %/T are obtained.

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Figure 5. Normalized deflection-quality factor of split-contact magnetoresistors with non-ideal split contacts $dd = 0.4 \,\mu m @ N_D = 5E13 \, cm^{-3}$, L/W = 4 and $B = 1 \, T$.



Figure 6. Sensitivity of split-contact magnetoresistors with ideal $(dd = 0 \ \mu m)$ and non-ideal $(dd = 0.4 \ \mu m)$ split contacts @ L/W = 4 and $B = 1 \ T$.

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(b) Sensitivity of magneto-resistors of square geometry (L = W). The dimensions of the devices with doping concentration of $5E17 \, cm^{-3} \, (5E13 \, cm^{-3})$ are indicated on the top (bottom) horizontal scale.

Figure 7. Sensitivity of split-contact magnetoresistors with ideal split contacts $dd = 0 \ \mu m \ @ B = 1 T$.